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## **Low-bandgap small molecules for near-infrared photovoltaic applications**

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# Low-bandgap small molecules for near-infrared photovoltaic applications

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**Abstract.** We investigate the effects of interfacial layers on the photovoltaic properties of bilayer organic heterojunction photovoltaic devices. The devices were fabricated using aluminum phthalocyanine chloride (AlPcCl) as electron donor and fullerene (C<sub>60</sub>) as electron acceptor. Two types of interfacial layers inserted between the transparent indium-tin-oxide anode and the AlPcCl layer were investigated: PEDOT:PSS and MoO<sub>3</sub>. We find that these interfacial layers have a strong influence on the device open-circuit voltage ( $V_{OC}$ ). The effects of temperature and illumination intensity on  $V_{OC}$  were explored. © 2011 Society of Photo-Optical Instrumentation Engineers. [DOI: [10.1117/1.3528044](https://doi.org/10.1117/1.3528044)]

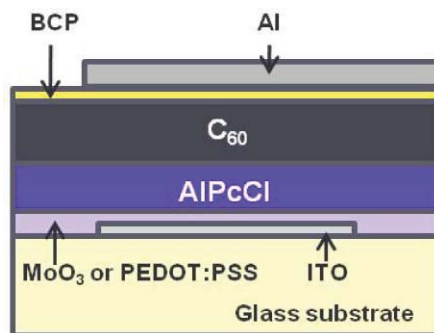
**Keywords:** organic photovoltaics; surface recombination; interfacial layers; open-circuit voltage.

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## 1 Introduction

Aluminum phthalocyanine chloride (AlPcCl) is a low-bandgap ( $E_g = 1.56$  eV) small-molecule organic semiconductor that is currently being explored to extend the spectral range of organic photovoltaic devices to the near-infrared. Recent works<sup>1-3</sup> on bilayer organic photovoltaic devices using AlPcCl as the donor molecule combined with C<sub>60</sub> as the acceptor molecule have demonstrated 2% power conversion efficiency in these devices. In these works, the type of interfacial layer formed at the indium-tin-oxide (ITO) anode was shown to have a strong influence on the device open-circuit voltage ( $V_{OC}$ ). UV ozone treated ITO substrates manifested substantially different  $V_{OC}$  of 0.68 V (Ref. 1) and 0.84 V (Ref. 2). In devices where molybdenum oxide (MoO<sub>3</sub>) was used as an interfacial layer,  $V_{OC} = 0.83$  V has been reported.<sup>3</sup>

In general, the power conversion efficiency ( $\eta_p$ ) of a photovoltaic device is given by  $\eta_p = V_{OC}J_{SC}FF/P_{in}$  where  $J_{SC}$  and FF are the device short-circuit current density and fill factor, respectively, and  $P_{in}$  is the incident light intensity. Aside from its direct effect on  $\eta_p$ ,  $V_{OC}$  is also known to have an influence on FF. Shockley and Queisser<sup>4</sup> were the first to note that FF for an ideal solar cell depends only on the temperature normalized open-circuit voltage,  $v_{OC} = V_{OC}/(k_B T/q)$ , where  $T$  is the cell temperature,  $k_B$  is Boltzmann's constant, and  $q$  is the electronic charge. Empirical expressions proposed by Green<sup>5</sup> demonstrated that FF increases as  $v_{OC}$  is raised. Therefore, in order to optimize the efficiency of AlPcCl-based bilayer organic photovoltaic devices, it is important to understand the observed effects<sup>1-3</sup> of the anode interface on  $V_{OC}$ . In the present work, we address the question of whether the device open-circuit voltage is determined by the intrinsic properties of the AlPcCl/C<sub>60</sub> donor/acceptor heterojunction or the properties of the electrode interfaces. From detailed temperature and power dependence of



**Fig. 1** Structure of the bilayer devices based on small molecules AIPcCl (donor) and  $C_{60}$  (acceptor).

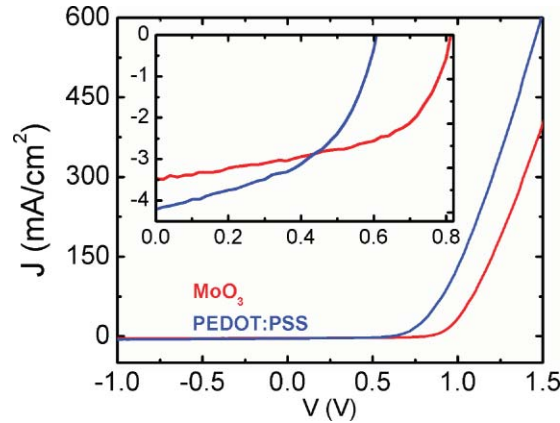
the device current density versus voltage characteristics, we show that both factors contribute to the device open-circuit voltage.

## 2 Device Fabrication and Characterization

The materials used to fabricate our bilayer devices were acquired from various commercial sources. The device geometry is presented in Fig. 1. The substrate is glass covered with transparent conducting ITO ( $\sim 150$  nm thick with sheet resistance  $R_s = 4\text{--}8 \Omega$  from Delta Technologies). We investigated poly(3,4-ethylenedioxythiophene) doped with poly(styrenesulfonate) (PEDOT:PSS) in aqueous solution (Baytron P, H.C. Stark, USA) and  $MoO_3$  (Aldrich, USA) as interfacial hole-transport layers in our devices. Sublimed grade bathocuproine (BCP, Aldrich) was used to form an ohmic contact between  $C_{60}$  and the aluminum electrode. AIPcCl (Aldrich) and  $C_{60}$  (99.5% purity, nano-C) were used to form the electroactive bilayers of our devices. AIPcCl was purified by thermal gradient sublimation before being used for device fabrication.

The ITO electrodes were first patterned on the glass substrates by photolithographic techniques. The ITO substrates were then cleaned by ultrasonic treatment sequentially in detergent, deionized water, and acetone followed by rinsing in isopropyl alcohol. To ensure a valid comparison of the photovoltaic characteristics of devices with different interfacial layers, substrates covered by PEDOT:PSS and  $MoO_3$  were initially prepared separately. A 50-nm-thick PEDOT:PSS film was spin-coated from the aqueous Baytron P solution onto the ITO/glass at 5000 rpm under ambient atmosphere. The air-dried film was transferred inside a glove box and heated at  $150^\circ\text{C}$  for 10 min to remove any residual moisture from the film. A 60-Å  $MoO_3$  thin film was thermally evaporated on another patterned ITO substrate. Both substrates were then loaded into the thermal evaporation system for subsequent depositions of the remaining identical layers in each device comprising the device structure. Films of 220 Å of AIPcCl and 425 Å of  $C_{60}$  were thermally evaporated onto the substrates with a base pressure of  $2 \times 10^{-6}$  Torr. The devices were completed by depositing 100 Å of BCP and a 1000 Å Al through a shadow mask defining the  $0.05 \times 0.05$ -in. square active area for the device. The entire device fabrication was carried out inside a nitrogen-filled glove box to avoid potential sources for photo-oxidative degradation.

On completion, the devices were mounted in a cryostat inside the glove box. The mounted device was subsequently taken outside the glove box and pumped to  $5 \times 10^{-6}$  Torr prior to measurement of the current density versus voltage ( $J$ - $V$ ) characteristics. The measurements were performed over a temperature range of 30–300 K and illumination intensities between 12 and  $194 \text{ mW}/\text{cm}^2$ . The illumination source was a simulated AM 1.5 global solar simulator (Oriol 300 W) with a maximum integrated intensity of  $\sim 200 \text{ mW}/\text{cm}^2$ . The incident illumination intensity was adjusted using different size apertures and by varying the power of the solar simulator. The intensity was measured using an NREL-calibrated silicon photovoltaic cell as detector.



**Fig. 2** Room-temperature  $J_L$ - $V$  characteristics of AlPcCl/ $C_{60}$  heterojunctions with the two types of interfacial layers,  $MoO_3$  and PEDOT:PSS, under AM1.5 global solar simulator with  $100 \text{ mW/cm}^2$ .

### 3 Results and Discussions

#### 3.1 Room-Temperature Current Density versus Voltage Characteristics in the Dark and under Illumination

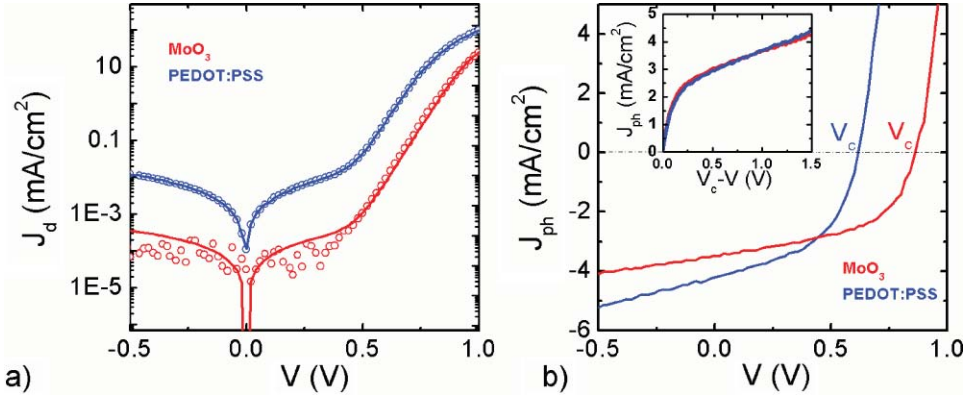
Figure 2 presents a comparison of the illuminated current density ( $J_L$ ) versus voltage ( $V$ ) characteristics at room temperature of the AlPcCl/ $C_{60}$ -based heterojunction photovoltaic devices fabricated with the two types of interfacial layers. We observe a significant increase in the open-circuit voltage from  $V_{OC} = 0.61 \text{ V}$  using the PEDOT:PSS interfacial layer to  $V_{OC} = 0.81 \text{ V}$  for the device with the  $MoO_3$  layer. The corresponding device fill factor also increased from 0.49 to 0.55. However, the short-circuit current is reduced for the device fabricated with  $MoO_3$  compared to PEDOT:PSS from 4.21 to 3.47  $\text{mA/cm}^2$ . Nevertheless, the observed increase in  $V_{OC}$  and FF results in a significant improvement in the power-conversion efficiency from 1.33 to 1.64%.

To understand the differences in the  $J$ - $V$  characteristics presented in Fig. 2, we use the typical equivalent circuit model developed to describe photovoltaic devices.<sup>6</sup> In this model, the photocell is described by a diode in parallel with a current source,  $J_{ph}$ , and a parallel resistance  $R_p$ , all connected in series with the resistance  $R_s$ . The diode represents the rectifying donor-acceptor heterojunction and is characterized by the reverse-bias saturation current density  $J_s$ , and the diode ideality factor  $n$ .  $J_{ph}(V)$  is the voltage-dependent photogenerated current density present in the device under illumination, and it becomes zero for devices measured in the dark. The parallel resistance  $R_p$  is related to leakage currents due to pinholes or other imperfections during device fabrication or to intrinsic recombination processes present in the active layers. The series resistance  $R_s$  accounts for the organic layer resistance together with the contact resistance formed between each of the interfaces present in the device. With this model, the current density ( $J$ ) as a function of the applied voltage is given by the generalized Shockley diode Eq. (1),

$$J = \frac{R_p}{R_s + R_p} \left\{ J_s \left[ \exp \frac{q(V - J R_s)}{n k_B T} - 1 \right] + \frac{V}{R_p} \right\} - J_{ph}(V). \quad (1)$$

Note that Eq. (1) describes the illuminated current density ( $J_L$ ) when  $J_{ph} \neq 0$  and the dark current density ( $J_d$ ) for  $J_{ph} = 0$ . In our analysis, we estimate the photocurrent as  $J_{ph} = J_L - J_d$ .

The experimental  $J_d$  versus  $V$  curve is fitted to Eq. (1) to obtain the diode parameters  $R_s$ ,  $R_p$ ,  $n$ , and  $J_s$ . The fit to the room temperature  $J_d - V$  for both devices is presented in Fig. 3. Good agreement of the fit with the data is obtained using the diode parameters listed in the caption to Fig. 3. When the PEDOT:PSS interfacial layer is replaced with the  $MoO_3$  interfacial layer,



**Fig. 3** (a) Dark  $J_d$ - $V$  characteristics of AIPcCl/C<sub>60</sub> heterojunction devices fabricated with two types of interfacial layers: MoO<sub>3</sub> and PEDOT:PSS. The lines represent fits to the data using Eq. (1) with fitting parameters:  $J_s = 7.84 \times 10^{-9}$  mA/cm<sup>2</sup>,  $n = 1.69$ ,  $R_s = 1.84 \Omega \text{ cm}^2$ ,  $R_p = 1.39 \text{ M}\Omega \text{ cm}^2$  for the MoO<sub>3</sub> device, and  $J_s = 9.48 \times 10^{-7}$  mA/cm<sup>2</sup>,  $n = 1.82$ ,  $R_s = 1.36 \Omega \text{ cm}^2$ ,  $R_p = 0.48 \text{ M}\Omega \text{ cm}^2$  for the PEDOT:PSS device. b)  $J_{ph}$ - $V$  characteristics of AIPcCl/C<sub>60</sub> heterojunction devices fabricated with two types of interfacial layers: MoO<sub>3</sub> and PEDOT:PSS. Inset:  $J_{ph}$  as a function of effective applied voltage,  $V_c - V$ , where  $V_c$  is the compensation voltage defined in the text.

the reverse-bias saturation current  $J_s$  decreases by two orders of magnitude from  $9.48 \times 10^{-7}$  mA/cm<sup>2</sup> to  $7.84 \times 10^{-9}$  mA/cm<sup>2</sup>. As we will show later, such a decrease in  $J_s$  can explain the elevated  $V_{OC}$  measured from the device with the MoO<sub>3</sub> interfacial layer.

An expression for the  $V_{OC}$  can be extracted from Eq. (1) by setting  $J = 0$ . For  $R_s \ll R_p$  this yields,

$$V_{oc} = \frac{nk_B T}{q} \ln \left( \frac{J_{ph}(V_{oc})}{J_s} + 1 - \frac{V_{oc}}{J_s R_p} \right). \quad (2)$$

The device fill factor can also be calculated from the diode parameters of Eq. (1). In general, FF is obtained numerically. However, the following empirical estimates were previously shown to be good approximations of the numerical values when  $V_{OC} > 10nk_B T$ <sup>5,6</sup>,

$$\begin{aligned} FF_O &= \frac{v_{OC} - \ln(v_{OC} + 0.72)}{v_{OC} + 1}, \quad (r_s = 1/r_p = 0) \\ FF_S &= FF_O (1 - 1.1r_s) + 0.19r_s^2, \quad (0 \leq r_s \leq 0.4, 1/r_p = 0) \\ FF &= FF_S \left\{ 1 - \frac{(v_{OC} + 0.7) FF_S}{v_{OC} r_p} \right\}, \quad (0 \leq r_s + 1/r_p \leq 0.4) \end{aligned} \quad (3)$$

where the normalized quantities are defined as  $v_{OC} = qV_{OC}/nk_B T$ ,  $r_s = R_s/R_{CH}$ , and  $r_p = R_p/R_{CH}$ . The characteristic resistance is given by  $R_{CH} = V_{OC}/J_{SC}$ .

We compare the experimentally measured  $V_{OC}$  with that given by Eq. (2) using the fitting parameters obtained from the dark current characteristics described above. From Fig. 3(b), we estimate  $J_{ph}(V_{OC}) = 1.16$  mA/cm<sup>2</sup> for the MoO<sub>3</sub> device and  $J_{ph}(V_{OC}) = 0.31$  mA/cm<sup>2</sup> for the PEDOT:PSS device. Using Eq. (2), and noting that the first term dominates over the other two terms for the quantities inside the bracket, the expected open-circuit voltage for the device with a PEDOT:PSS interface is  $V_{OC} = 0.60$  V, whereas the one with a MoO<sub>3</sub> interface has  $V_{OC} = 0.82$  V. These estimates are in very good agreement with the experimental values of 0.61 and 0.81 V, respectively, suggesting that the equivalent circuit model is applicable in describing the devices' photovoltaic characteristics at room temperature.

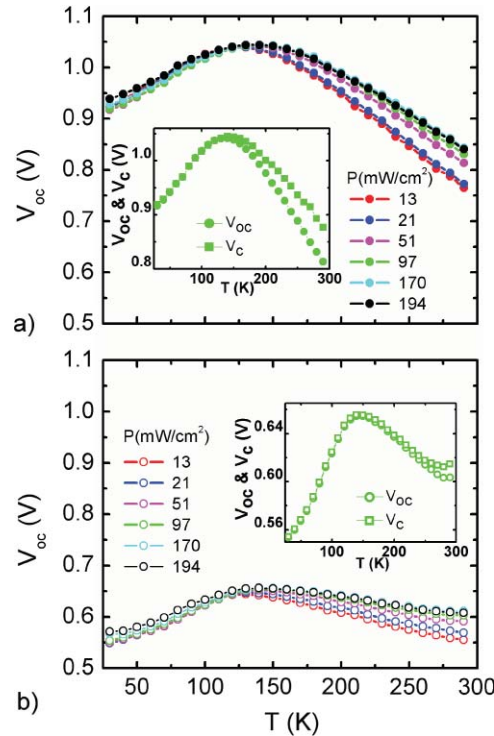
We now account for the observed fill factor in both devices. Using the estimate of  $V_{OC}$  derived from the dark diode characteristics, the ideal fill factor ( $FF_0$ ) calculated from Eq. (3) is  $FF_0 = 0.80$  for the  $MoO_3$  device and  $FF_0 = 0.74$  for the PEDOT:PSS device. Correction associated with the different series resistance yields  $FF_S = 0.79$  for the  $MoO_3$  device and  $FF_S = 0.73$  for the PEDOT:PSS device, demonstrating negligible effect of  $R_s$  on FF. The large value of  $R_p$  extracted from the dark  $J_d-V$  characteristic from both devices also results in negligible correction to the fill factor. However, the linear increase of  $J_{ph}$  at large negative applied voltage [seen in Fig. 3(b)] suggests another  $R_p$  contribution to FF under illumination condition. Estimating this light-induced parallel resistance from the slope of the linear part of the  $J_L-V$  curve, we obtain  $R_p \approx 850 \Omega \text{ cm}^2$  for the  $MoO_3$  device and  $R_p \approx 538 \Omega \text{ cm}^2$  for the PEDOT:PSS device. Using these values, the fill factor calculated from Eq. (3) is  $FF = 0.61$  for the  $MoO_3$  device and  $FF = 0.55$  for the PEDOT:PSS device, values that are comparable to the corresponding measured device fill factor. This analysis shows that FF is controlled by the ideality factor and saturation current of the diode as well as a light-induced  $R_p$  contribution. The latter could come from photoconductivity of the donor and/or acceptor layers.<sup>7</sup>

The measured  $J_{ph}$  versus  $V$  characteristics for the two different interfacial devices under investigation are presented in Fig. 3(b). In the inset of Fig. 3(b),  $J_{ph}$  is plotted against the effective voltage across the device,  $V_C-V$ , where  $V_C$  is the compensation voltage defined as the voltage where  $J_{ph} = 0$ .  $V_C$  is 0.62 V for device fabricated with a PEDOT:PSS interfacial layer, while  $V_C = 0.86$  V for a  $MoO_3$  interfacial layer device. We note that a scaling factor of 0.75 was used to multiply  $J_{ph}$  for the  $MoO_3$  devices. Surprisingly, the shape of the photocurrent for both devices is nearly identical demonstrating that the photocurrent generated within the device is determined by the effective voltage,  $V_C-V$ , consistent with the absence of space-charge formation in the donor and acceptor layers. Thus, the differences that we observe in the  $J_{ph}-V$  curves can be attributed to the differences in the built-in field imposed by the presence of the anode interfacial layers. To gain further insight into the origin of the  $V_{OC}$ , we explore the photovoltaic characteristics of both devices at various temperatures and intensities of the incident light.

### 3.2 Temperature and Power Dependence of the Open-Circuit Voltage

Figure 4 compares the temperature dependence of the open-circuit voltage for both devices under different illumination intensities. For a given incident illumination intensity, we observe a linear increase in  $V_{OC}$  as the temperature decreases from 300 to 140 K. A maximum value for  $V_{OC}$  is achieved at  $\sim 140$  K in both devices. Figure 4 shows this value is 1.05 V for the device fabricated with  $MoO_3$  layer [Fig. 4(a)], whereas it is 0.65 V for the device with the PEDOT:PSS interfacial layer [Fig. 4(b)]. These observations indicate that the maximum  $V_{OC}$  value is strongly dependent on the nature of the anodic interfacial layer, while its position on the temperature scale seems to be determined by the properties of the donor/acceptor heterojunction. Upon further cooling, we observe a decrease in  $V_{OC}$  for both devices. The insets show the comparison of the temperature dependence of  $V_{OC}$  and the compensation voltage,  $V_C$ , in both devices.  $V_{OC}$  coincides with  $V_C$  for  $T < 140$  K with both decreasing by nearly the same value of  $\sim 0.1$  V at the lowest temperature. For  $T > 140$  K,  $V_{OC} < V_C$  with the  $MoO_3$  device manifesting a larger offset than that of the PEDOT:PSS device.

Figure 4 also reveals a clear dependence of  $V_{OC}$  on the incident light intensity that is observed for  $T > 140$  K in both devices. At  $< 140$  K, this power dependence disappears. Figure 5(a) presents a semilogarithmic plot of  $V_{OC}$  versus  $P$ , where  $P$  is the incident light intensity at three representative temperatures. The experimental data can be fitted with a linear function, and the slope can be compared to  $k_B T/q$ . The extracted slope decreases rapidly with temperature from  $1.20 k_B T/q$  ( $0.80 k_B T/q$ ) at  $T = 290$  K to  $0.92 k_B T/q$  ( $0.69 k_B T/q$ ) when  $T = 200$  K and  $0.52 k_B T/q$  ( $0.47 k_B T/q$ ) at  $T = 150$  K for the  $MoO_3$  (PEDOT:PSS) device. Equation (2) relates the observed power dependence of  $V_{OC}$  to that of  $J_{ph}(V_{OC})$ . Assuming that the measured photocurrent at  $V = V_{OC}$  obeys the power-law dependence,  $J_{ph}(V_{OC}) = J_T(P/P_0)^\alpha$ , where the parameter  $J_T$



**Fig. 4** Open-circuit voltage as a function of temperature for AlPcCl/C<sub>60</sub> devices with (a) MoO<sub>3</sub> and (b) PEDOT:PSS interfacial layers under AM 1.5 Global solar simulator with various incident power intensity. The inset compares the temperature dependence of the open-circuit voltage ( $V_{OC}$ ) and the compensation voltage ( $V_C$ ) for  $P = 97$  mW/cm<sup>2</sup>.

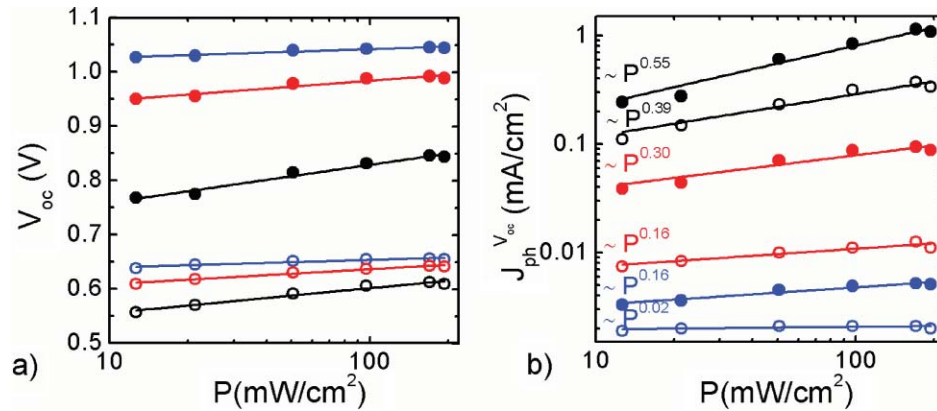
depends only on temperature, then  $V_{OC}$  is given by

$$V_{OC} \simeq \frac{nk_B T}{q} \ln \left( \frac{J_T (P/P_0)^\alpha}{J_s} \right) = \frac{nk_B T}{q} \left( \alpha \ln \frac{P}{P_0} + \ln \frac{J_T}{J_s} \right). \quad (4)$$

Figure 5(b) shows a double-logarithmic plot of  $J_{ph}(V_{OC})$  versus  $P$ . We observe an experimental power law dependence of  $J_{ph}(V_{OC})$  with the exponent strongly decreasing with temperature. Extracting  $\alpha$  from Fig. 5(b) and combined with the slope of  $V_{OC}$  versus  $\ln(P)$  determined from Fig. 5(a), the diode ideality factor can be obtained using Eq. (4). The results of this analysis at various temperatures and their comparison to  $n$  derived from the  $J_d$  versus  $V$  characteristics are displayed in Fig. 6. Good agreement between the two values of  $n$  is illustrated in Fig. 6, corroborating our assumption of the power-law dependence of  $J_{ph}(V_{OC})$  with  $P$  as well as demonstrating that the equivalent circuit model is a good representation of the data.

### 3.3 Discussion

We have shown above that the observed variation in  $V_{OC}$  associated with different interfacial layers at the anode of AlPcCl/C<sub>60</sub> bilayer organic photovoltaic devices is related to the diode saturation current density  $J_s$ . Earlier works on inorganic  $p$ - $n$  homojunctions and heterojunctions have shown that  $J_s$  results from the dominant transport process associated with the  $p$ - $n$  junction.<sup>8</sup> For devices with finite thickness, recombination at the electrode interfaces can also influence  $J_s$ . In  $p$ - $n$  homojunctions, finite thickness correction leads to  $J_s = J_{s0} F$ , where  $J_{s0}$  is the saturation



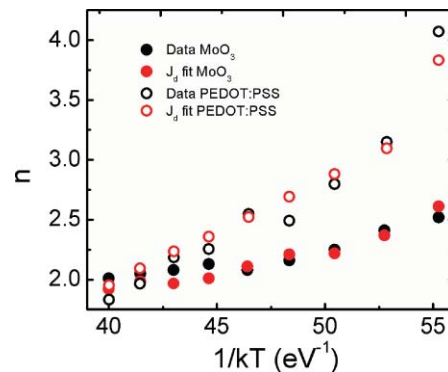
**Fig. 5** Incident power ( $P$ ) dependence of the open-circuit voltage ( $V_{OC}$ ) (a) and the photocurrent at  $V = V_{OC}$  [ $J_{ph}(V_{OC})$ ] at three representative temperatures:  $T = 290$  K (black),  $200$  K (red), and  $150$  K (blue). The solid circles are for the  $\text{MoO}_3$  device, and the open-circles are for the PEDOT:PSS device.

current density for an infinitely thick diode and

$$F = \frac{S \cosh(W/L) + (D/L) \sinh(W/L)}{(D/L) \cosh(W/L) + S \sinh(W/L)}, \quad (5)$$

where  $W$  is the depletion width associated with the band-bending at the  $p$ - $n$  junction,  $S$  is the surface recombination velocity at the electrode interface, and  $D$  and  $L$  are the diffusion coefficient and diffusion length of the minority carrier at the interface.<sup>9</sup> Applying Eq. (5) for the organic heterojunction with  $W \ll L$  (Ref. 10), then  $J_s \approx (J_{SO}L/D)S$ . Recall that  $J_s$  is nearly two orders of magnitude lower in the device with the  $\text{MoO}_3$  interface than that with the PEDOT:PSS interface. In the approximate expression for  $J_s$ , the quantities  $J_{SO}$ ,  $L$ , and  $D$  are the same in both devices. Thus,  $S$  at the  $\text{MoO}_3/\text{AIClPc}$  interface is significantly lower than the one associated with the PEDOT:PSS/AIClPc interface. Such difference between the surface recombination velocities of the respective interfaces accounts for the variation in the open-circuit voltage observed in AIClPc/ $\text{C}_{60}$  bilayer photovoltaic devices.

An early work by Rand *et al.*<sup>7</sup> demonstrated that, in bilayer organic photovoltaic devices,  $V_{OC}$  approaches its maximum value at low temperatures. Our current work demonstrates that this maximum value coincides with the compensation voltage  $V_C$ . Malliaras *et al.*<sup>11</sup> showed that  $V_C$  at low temperatures is a measure of the diode built-in potential  $V_{bi}$ . We find that  $V_{bi}$  is higher



**Fig. 6** Comparison of the diode ideality factor obtained from the data in Fig. 5 using Eq. (4) and from the fit of the  $J_d$  versus  $V$  using Eq. (1).



in the device where MoO<sub>3</sub> is used as an interfacial layer. Neglecting excitonic corrections, the maximum  $V_{OC}$  (or  $V_{bi}$ ) in organic photovoltaic devices is given by the difference between the energetic positions of the donor highest-occupied molecular orbital ( $E_{HOMO}$ ) and the acceptor lowest-unoccupied molecular orbital ( $E_{LUMO}$ ) (Refs. 7 and 12). Measurements using ultraviolet photoelectron spectroscopy report values of 5.3 eV (Ref. 2) and 5.4 eV (Ref. 1) for  $E_{HOMO}$  in AlPcCl and 4.1 eV (Ref. 13) and 4.5 eV (Refs. 1 and 2) for  $E_{LUMO}$  in C<sub>60</sub>. These values suggest that the maximum attainable  $V_{OC}$  for AlPcCl/C<sub>60</sub> heterojunction devices is  $\sim 0.8$  to 1.3 V. The data in Fig. 4 illustrate that this expected maximum  $V_{OC}$  is achieved in the MoO<sub>3</sub> device in which it is observed that  $V_{OC} = 1.05$  V at  $T = 140$  K, indicating negligible voltage losses at the MoO<sub>3</sub>/AlPcCl interface. The observed higher maximum  $V_{OC}$  (and  $V_{bi}$ ) in the MoO<sub>3</sub> device compared to that in the PEDOT:PSS device is consistent with the low surface recombination velocity in the former as described earlier.

An unusual feature of the data presented in Fig. 4 is the apparent peak seen in the  $V_{OC}$  versus  $T$  curves at  $T = 140$  K in both devices. Both devices manifest a drop from this peak  $V_{OC}$  value by about  $\delta V_{OC} = 0.1$  V as the temperature is lowered to  $T = 30$  K, suggesting that the effect is associated with the  $p$ - $n$  heterojunction at the AlPcCl/C<sub>60</sub> interface. This observation indicates a voltage loss contribution of the AlPcCl/C<sub>60</sub> heterojunction to  $V_{OC}$ . We argue that the presence of photoexcited charge carriers at high temperatures screens the electrostatic band bending at this  $p$ - $n$  heterojunction reducing its deleterious effect on  $V_{OC}$ .

## 4 Conclusions

The variation in the open-circuit voltage associated with different anode interface layers in chloroaluminum phthalocyanine/fullerene bilayer organic photovoltaic devices is shown to arise from interface charge recombination rather than from the intrinsic properties of the AlPcCl/C<sub>60</sub> donor/acceptor heterojunction. Low surface recombination velocity is achieved at the interface formed by aluminum phthalocyanine chloride with molybdenum oxide accounting for the high  $V_{OC}$  in devices where MoO<sub>3</sub> is used as an interfacial layer.

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